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PATENT APPLICATION

ATTORNEY DOCKET NO. 10991888-1

IN THE U.S. PATENT AND TRADEMARK OFFICE Patent Application Transmittal Letter

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Charge \$ 930 to Deposit Account 08-2025. At any time during the pendency of this application, please charge any fees required or credit any over payment to Deposit Account 08-2025 pursuant to 37 CFR 1.25. Additionally please charge any fees to Deposit Account 08-2025 under 37 CFR 1.16, 1.17,1.19, 1.20 and 1.21. A duplicate copy of this sheet is enclosed.

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Date of Deposit <u>3/22/00</u>

I hereby certify that this is being deposited with the United States Postal Service "Express Mail Post Office to Addressee" service under 37 CFR 1.10 on the date indicated above and is addressed to: Assistant Commissioner for Patents, Washington, D.C. 20331.

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Respectfully submitted,

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HARDWARE MODELING OF LED RELATIVE BRIGHTNESS

CROSS REFERENCE TO RELATED APPLICATIONS

A related copending United States patent applications commonly owned by the assignee of the present document and incorporated by reference in its entirety into this document is being filed in the United States Patent and Trademark Office on or about the same day as the present application. This related application is Hewlett-Packard docket number 10002968, serial number ______, and is titled "SOFTWARE DETERMINATION OF LED BRIGHTNESS AND EXPOSURE."

FIELD OF THE INVENTION

The invention relates generally to precision control of an exposure and more particularly to modeling the light output of a light emitting diode (LED) to maintain a constant exposure as the light output of an array of LED's changes.

BACKGROUND OF THE INVENTION

High quality image capture such, as grayscale and color imaging, needs a precision light source. Because of their size, price, reliability, and other qualities, light emitting diodes (LED's) may be chosen as the light source for image capture. Unfortunately, the light output of an LED changes with junction temperature and age.

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Because LED's heat up when they are on, one of the factors that determines the junction temperature of an LED, and hence its light output, is the amount of time, and duty cycle, that the LED is on. One way to compensate for at least part of this variation is to use a light calibration strip. A light calibration strip may be used with a search algorithm to set the illumination levels prior to image capture. A disadvantage of this method is that part of the image capture array is used to sense the calibration strip. This decreases the width or area that is captured at any given moment. Another disadvantage is that this method does not account for changes in the junction temperature during image capture.

Accordingly, there is a need in the art for an illumination compensation method and apparatus that does not utilize a light calibration strip.

SUMMARY OF THE INVENTION

An embodiment of the invention provides, via simple electronic circuitry, an analog voltage that tracks the LED light output. This analog voltage is read to ascertain an approximate relative light output of the LED so that an exposure compensation can be quickly calculated. Since the analog voltage is generated via simple electronic circuitry, it is inexpensive to implement and does not require the calculation of difficult exponential equations that would require a relatively long time to calculate on an associated processor. In the preferred embodiment, a resistor-capacitor circuit is used to approximate the behavior of the LED light output. The output voltage from this circuit is sampled and used along with a sensed ambient temperature to adjust the capture exposure.

Other aspects and advantages of the present invention will become apparent from the following detailed description, taken in conjunction with the accompanying drawings, illustrating by way of example the principles of the invention.

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BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a block diagram of a capture exposure system.

FIG. 2 is a schematic diagram of an RC circuit that may be used to model LED relative light output.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

FIG. 1 is a block diagram of a capture exposure system 100. Central processing unit (CPU) 110 sends illumination control signal 116 to LED driver 112 and LED model 102. LED driver 112 is coupled to LED array 114. LED array 114 provides illumination for capturing an image. LED model provides analog voltage 118 that tracks the light output of the LED's in LED array 114. Analog voltage 118 is input to analog-to-digital converter (A/D converter) 104. The output of A/D converter 104 is read by CPU 110. This capture exposure system also has an ambient temperature sensor 106. The output of ambient temperature sensor 106 is read by A/D converter 104 and passed to CPU 110. CPU 110 uses these two values to calculate an exposure time for an image capture.

The light output of an LED can be described with the following equation using an experimentally derived figure-of-merit T₀:

$$RLOP(T) \equiv e^{\left[\frac{-(T-T_c)}{T_0}\right]}$$
 Equation 1

where RLOP(T) is the relative light output when the p-n junction is at temperature T. T_c is the reference temperature that the relative light output is reference to. In other words, RLOP(T_c)=1. T_0 is determined by measuring the relative light output at numerous junction temperatures and then applying an exponential fit to determine the T_0 for that particular device. The above equation describes relative light output in terms of the p-n junction temperature. Unfortunately, this temperature

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depends on a number of other factors including the ambient temperature, the on-off history of the LED, the forward voltage, forward current, LED efficiency, and the thermal time constant of the LED. The on-off history of the LED is particularly important because it determines the starting temperature of the LED each time it is turned on or turned off. When an LED is on, the junction temperature follows a heating curve that resembles:

$$T_{j} = \left(T_{\infty} - T_{on}\right) \left[1 - e^{\frac{-t}{\tau}}\right] + T_{on}$$
 Equation 2

where T_{on} is the starting temperature of the junction when the LED is turned on, T_{oc} is the steady-state junction temperature that the junction would reach after the LED is on a long time and τ is the thermal time constant of the LED. When an LED is off, the junction temperature follows a cooling curve that resembles:

$$T_i = (T_{off} - T_a)e^{\frac{-t}{\epsilon}} + T_a$$
 Equation 2

where T_{off} is the starting temperature of the junction when the LED is turned off, T_a is the ambient air temperature and τ is the thermal time constant of the LED. Substituting Equation 2 into Equation 1 to produce an equation that relates

$$RLOP(t_{cor}) = K_1 e^{K_2 e^{(-t/\tau)}}$$
 Equation 4

relative light output to on time, the result has the form:

where:

$$K_1 = e^{\left[\frac{T_e - T_o}{T_o}\right]}$$
 Equation 5

$$K_2 = \left[\frac{T_{\infty} - T_{on}}{T_0} \right].$$
 Equation 6

Note that since T_{∞} is the steady state value for the junction temperature, in normal operation $T_{\infty} \geq T_{on}$ so that K_2 will always be greater than or equal to zero.

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Accordingly, as on time, t_{on} , goes from zero to infinity, the RLOP decreases from K_1 -exp(K_2) to K_1 along a curve that has the shape of an exponential to a positive exponential to a negative x (i.e. exp(exp(-t))). Also note that if constant power is input to the LED, T_∞ will be a fixed amount above the ambient air temperature T_a .

This allows K_1 and K_2 to be expressed in terms of the ambient air temperature, T_a , and another constant, T_{Δ} . T_{Δ} is the temperature rise above ambient that the LED junction is at for a given power input, thermal resistance, and efficiency. Accordingly, K_1 and K_2 may be expressed as:

$$K_1 = e^{\left[\frac{T_c - T_a - T_A}{T_0}\right]} = e^{\frac{-T_A}{T_0}} \cdot e^{\left[\frac{T_c - T_a}{T_0}\right]}$$
 Equation 7

$$K_2 = \left\lceil \frac{T_a + T_{\Delta} - T_{on}}{T_c} \right\rceil$$
 Equation 8

Substituting equation 3 into equation 1 to produce an equation that relates relative light output to off time, the result has the same form as Equation 4 but different constants:

$$RLOP(t_{eff}) = K_3 e^{K_4 e^{(-t/\tau)}}$$
 Equation 9

where:

$$K_{3} = e^{\left[\frac{T_{c} - T_{a}}{T_{b}}\right]}$$
 Equation 10

$$K_4 = \left\lceil \frac{T_a - T_{off}}{T_0} \right\rceil.$$
 Equation 11

Note that T_a is the steady state value for the junction temperature if the LED is off for a very long time and that in normal operation $T_{eff} \ge T_a$. This means that K_4 will always be less than or equal to zero. Accordingly, as off time, t_{eff} , goes from zero to infinity, the RLOP increases from K_3 exp(K_4) (which is less or equal to K_3 since

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 $K_4\le 0$) to K_3 along a curve that has the shape of an exponential to a negative exponential to a negative x (i.e. exp(-exp(-t))).

Equations 3 and 9 both have the form:

$$RLOP(t) = K_a e^{K_b e^{(-t/t)}}$$
 Equation 12

The Taylor series expansion of Equation 12 is:

$$K_a e^{K_b e^{(-t/\tau)}} = K_a \left[1 + K_b e^{(-t/\tau)} + \frac{K_b^2 e^{(-2t/\tau)}}{2!} + \frac{K_b^3 e^{(-3t/\tau)}}{3!} + \cdots \right] \quad \text{Equation 13}$$

Since the exponent is negative in all the $e^{(...)}$ terms of the Taylor series expansion, they rapidly diminish in magnitude when $t > \tau$ or $|K_b| < 1$. Therefore, when either of these conditions is true, Equation 12 can be approximated by:

$$RLOP(t) = K_a e^{K_b e^{(-t/\tau)}} \approx K_a \left[1 + K_b e^{(-t/\tau)} \right]$$
 Equation 14

Applying this same approximation to Equations 3 and 9 yields:

$$RLOP(t_{on}) = K_1 e^{K_2 e^{(-t/\tau)}} \approx K_1 \left[1 + K_2 e^{(-t/\tau)}\right] = K_1 + K_1 K_2 e^{(-t/\tau)}$$
 Equation 15

$$RLOP(t_{off}) = K_3 e^{K_4 e^{(-t/\tau)}} \approx K_3 [1 + K_4 e^{(-t/\tau)}] = K_3 + K_3 K_4 e^{(-t/\tau)}$$
Equation 16

From the form of Equation 15, it can be seen that the relative light output while the LED is on will decrease in approximately an exponential fashion eventually approaching a limit value of K_1 . The amount of decrease is set by the initial temperature of the junction, T_{on} , each time the LED is turned on. T_{on} is embedding in K_2 . Likewise, it can be seen from the form of Equation 16 that the relative light output when the LED is next turned on increases along a curve similar to $1-e^x$ while the LED is off (because K_4 is always negative) eventually approaching a limit value of K_3 . The amount of increase is set by the initial temperature of the junction, T_{off} , each time the LED is turned off. T_{off} is embedded in K_4 . Finally, it is known that the relative light output does not change discontinuously at the instant the LED is turned

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on or off. Therefore, the initial conditions in K_2 and K_4 must be such that Equation 15 and Equation 16 are equal at each on-to-off and off-to-on transition.

The curves followed by Equations 15 and 16 have the same shape as the voltage across a capacitor being charged and discharged through a resistor. Likewise, a the voltage across a capacitor being charged and discharged does not change discontinuously during charging-to-discharging and discharging-to-charging transitions. Given these two conditions, the changes in the relative light output as an LED is switched on and off are modeled by this invention as a resistor-capacitor (RC) or inductor-resistor (LR) circuit. To model the relative light output with an RC circuit, the capacitor is charged through the resistor when the LED is off and discharged through the resistor when the LED is on. This RC model is shown in FIG. 2.

In FIG. 2, illumination control signal 116 is connected to a first terminal of resistor 202. The second terminal of resistor 202 is connected to the model output. The model output is analog voltage 118 that goes to the input of A/D converter 104. The second terminal of resistor 202 is also connected to the first terminal of capacitor 204. The second terminal of capacitor 204 is connected to the negative supply rail or some other reference voltage.

Illumination control signal 116 discharges capacitor 204 through resistor 202 when illumination control signal 116 is in a state that turns LED array 114 on. In FIG. 2, this is shown as a direct connection. However, depending on the polarity of the illumination control signal 116 a logical inversion or buffering may be necessary before it is applied to resistor 202.

To model the relative light output, an embodiment of the invention first charges the RC circuit to a known voltage level. This sets the initial condition of the

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model. This initial condition would normally be higher than the eventual discharged condition of the RC circuit because it is assumed that the LED junction is at the ambient air temperature and hence the relative light output is at its greatest level. Accordingly, the initial voltage across the capacitor of the RC circuit is at its greatest level when the relative light output is expected to be at its greatest level. During operation of the model, whenever the LED is on, the capacitor of the RC circuit is discharged through the resistor and whenever the LED is off, the capacitor of the RC circuit is charged through the resistor. This functions such that the voltage across the capacitor of the RC circuit tracks the change in relative light output from the relative light output when the LED junction was at the ambient temperature.

In an embodiment of the invention, the values for the resistor and capacitor are determined experimentally. A voltage level is arbitrarily chosen for the initial condition of the RC circuit that represents the light output when the LED brightest. To simplify design, this can be the positive power supply voltage. Likewise, a voltage level is arbitrarily chosen for the discharged state of the RC circuit that represents the light output when the LED is dimmest. To simplify design, this can be when the capacitor is fully discharged. The range of relative light output values that these two extremes represent is determined by the thermal properties of the entire illumination system and its packaging so this range is determined experimentally in the preferred embodiment.

When capture exposure system 100 is about to start an exposure it samples the voltage across capacitor 204 with A/D converter 104. This gives the system a modeled relative brightness. This modeled relative brightness is used along with a sampled ambient temperature to determine an exposure. The mapping of ambient temperature and modeled relative brightness to actual relative brightness performed

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by a lookup table in the preferred embodiment. The values of this lookup table may be determined experimentally or they may be calculated.

To calculate the values of this lookup table, Equation 1 is used as a starting point.

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$$RLOP(T) \equiv e^{\left[\frac{-(T-T_{\epsilon})}{T_{0}}\right]}$$
 Equation 1

Re-writing T, which is the junction temperature, in terms of T_a , T_Δ and a difference from maximum temperature factor, Δ_{T_c} produces:

$$T = T_{\infty} - \Delta_{\tau} = T_{\alpha} + T_{\Lambda} - \Delta_{\tau}$$
 Equation 17

substituting Equation 17 into Equation 1 produces:

$$RLOP(T) = e^{\left[\frac{-(T_a + T_b - \Delta_T - T_e)}{T_0}\right]}.$$
 Equation 18

Since all the factors in Equation 18 except T_a are constant for different ambient temperatures, then the relative light output at an ambient temperature T_{a1} can be related to the relative light output at an ambient temperature T_{a2} for the same Δ_T by:

$$LUT(T_{a2} - T_{a1}) = \frac{RLOP(T_{a2} + T_{\Delta} - \Delta_T - T_c)}{RLOP(T_{a1} + T_{\Delta} - \Delta_T - T_c)} = e^{T_{a2} - T_{a1}}$$
 Equation 19

Equation 19 can be used to construct a look-up table that produces a factor that is multiplied by the modeled relative brightness. The result of this multiplication produces actual relative brightness. This actual relative brightness is then used to calculate a capture exposure. One simple method of calculating the capture exposure is to divide the relative brightness by an exposure constant to produce an exposure time. Since the capture exposure is the total amount of light output by the LED integrated over time, this simple method produces a reasonably constant capture exposure over the range of LED brightness.

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In the preferred embodiment, the capture exposure is adjusted by turning the LED array on for the capture exposure time. However, other methods of adjusting the capture exposure, such as opening and closing a shutter, may be used.

From the foregoing it will be appreciated that the capture exposure system and LED relative brightness model provided by the invention offers the advantages of simplicity and avoids the calculation of difficult exponential equations or continuos integration by the control microprocessor. Furthermore, the system may be configured to a variety of thermal parameters or adapted to a variety of exposure control mechanisms.

Although several specific embodiments of the invention have been described and illustrated, the invention is not to be limited to the specific forms or arrangements of parts so described and illustrated. The invention is limited only by the claims.

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CLAIMS

What is claimed is:

- 1. An image capture device, comprising:
- an illumination source:
- a model of said illumination source having a model output; and, an exposure adjustment that is changed to compensate for changes in said illumination source as indicated by said model output.
- The image capture device of claim 1 wherein said model has a model input
 and said model input is an indication of the on times and the off times of said
 illumination source.
 - 3. The image capture device of claim 2, further comprising: an ambient temperature sensor producing a sensed ambient temperature wherein said exposure adjustment is also changed to compensate for said sensed ambient temperature.
 - The image capture device of claim 3 wherein said illumination source is at least one light emitting diode.
 - The image capture device of claim 4 wherein said model of said illumination source comprises a capacitor and a resistor.
- The image capture device of claim 4 wherein said model of said
 illumination source comprises an inductor and a resistor.

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- The image capture device of claim 4 wherein said exposure adjustment changes said on times of said illumination source.
- 8. A method of compensating for changes in an illumination source.
- 5 comprising:

modeling said illumination source; and,

adjusting an exposure to compensate for changes in said illumination source as indicated by said modeling.

- The method of claim 8 wherein said modeling has an input that is an indication of the on times and the off times of said illumination source.
 - 10. The method of claim 9 further comprising: sensing an ambient temperature; and,
- adjusting said exposure to compensate for said ambient temperature.
 - 11. The method of claim 10 wherein said illumination source is at least one light emitting diode.
- 20 12. The method of claim 11 wherein said modeling is performed by charging and discharging a capacitor.
 - The method of claim 12 wherein said charging and discharging is done through at least one resistor.

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14. The method of claim 11 wherein said modeling is performed by energizing and de-energizing an inductor.

- 15. The method of claim 14 wherein the rate of energizing and de-energizing is determined by at least one resistor.
 - 16. An article of manufacture comprising a program storage medium having computer readable program code means embodied therein for causing the adjustment of an exposure, the computer readable program code means in said article of manufacture comprising:

computer readable program code means for causing a computer to read an indication of an illumination sources brightness from a model;

computer readable program code means for causing said computer to adjust said exposure based on said indication of said illumination sources brightness.

17. The article of manufacture of claim 16 further comprising:

computer readable program code means for causing said computer to turn on and turn off said illumination source.

18. The article of manufacture of claim 17 further comprising:

computer readable program code means for causing said computer to indicate to said model the on times and off times of said illumination source.

19. The article of manufacture of claim 18 further comprising:

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computer readable program code means for causing said computer to obtain an indication of an ambient temperature; and,

computer readable program code means for causing said computer to adjust said exposure based on said indication of said ambient temperature.

- 20. The article of manufacture of claim 19 wherein said illumination source is at least one light emitting diode.
- 21. The article of manufacture of claim 20 wherein said model is a series resistor-capacitor circuit and said indication of said illumination sources brightness is obtained from the voltage across said capacitor.
- The article of manufacture of claim 20 wherein said model is a series resistor-inductor circuit.
 - 23. An image capture device, comprising:

illumination means:

modeling means, said modeling means producing a modeling means output
that is indicative of said illumination means relative brightness; and,
exposure adjustment means for changing and exposure to compensate for
changes in said relative brightness of said illumination means as
indicated by said modeling means output.

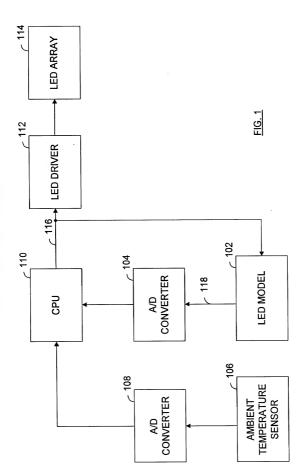
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- 24. The image capture device of claim 23 wherein said modeling means has a modeling means input and said modeling means input is an indication of the on times and the off times of said illumination means.
 - 25. The image capture device of claim 24, further comprising: ambient temperature sensor means for producing a sensed ambient temperature wherein said exposure is also changed to compensate for said sensed ambient temperature.
- 26. The image capture device of claim 25 wherein said illumination means is at least one light emitting diode.
- 27. The image capture device of claim 26 wherein said modeling means comprises at least a capacitor and a resistor.
- 28. The image capture device of claim 26 wherein said modeling comprises at least an inductor and a resistor.
- 29 The image capture device of claim 26 wherein said exposure is adjusted by
 changing said on times of said illumination source.

ABSTRACT

Via simple electronic circuitry, an analog voltage that tracks the LED light output is produced. This analog voltage is read by an A/D converter to ascertain an approximate relative light output of the LED so that light output compensation can be quickly calculated. A resistor-capacitor circuit is used to approximate the behavior of the LED light output. The output voltage from this circuit is sampled and used along with a sensed ambient temperature to adjust the exposure time of an image capture system.



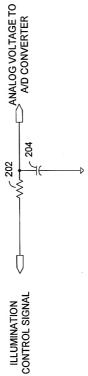


FIG. 2

DECLARATION AND POWER OF ATTORNEY FOR PATENT APPLICATION

ATTORNEY DOCKET NO. 10991888-1

As a below named inventor, I hereby declare that:

My residence/post office address and citizenship are as stated below next to my name;

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled:

Hardware	Modeling	Of LED	Relative	Brightness

The second of th	
the specification of which is attached	hereto unless the following box is checked:
•	•
() was filed on	as US Application Serial No. or PCT International Application
() was med on	
Number and was am	nended on (if applicable).
allu was all	(if applicable).

I hereby state that I have reviewed and understood the contents of the above-identified specification, including the claims, as amended by any amendment(s) referred to above. I acknowledge the duty to disclose all information which is material to patentability as defined in 37 CFR 1.56.

Foreign Application(s) and/or Claim of Foreign Priority

I hereby claim foreign priority benefits under Title 35, United States Code Section 119 of any foreign application(s) for patent or invertor(s) certificate listed below and have also identified below any foreign application for patent or inventor(s) certificate having a filing date before that of the application on which priority is claimed:

COUNTRY	APPLICATION NUMBER	DATE FILED	PRIORITY CLAIMED UN	IDER 35 U.S.C. 119
N/A			YES:	NO:
			YES:	NO:

Provisional Application

I hereby claim the benefit under Title 35, United States Code Section 119(e) of any United States provisional application(s) listed below:

APPLICATION SERIAL NUMBER	FILING DATE
N/A	

U. S. Priority Claim

I hereby claim the benefit under Title 35, United States Code, Section 120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code Section 112, I acknowledge the duty to disclose material information as defined in Title 37, Code of Federal Regulations, Section 1.56(a) which occurred between the filling date of the prior application and the national or PCT international filling date of this application.

APPLICATION SERIAL NUMBER	FILING DATE	STATUS (patented/pending/abandoned)
N/A		

POWER OF ATTORNEY:

As a named inventor, I hereby appoint the following attorney(s) and/or agent(s) to prosecute this application and transact all business in the Patent and Trademark Office connected therewith:

Customer Number 022879	Place Customer Number Bar Code Label here
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Send Correspondence to: HEWLETT-PACKARD COMPANY Intellectual Property Administration P.O. Box 272400 Fort Collins, Colorado 80528-9599 Direct Telephone Calls To: Alexander J Neudeck

(970) 898-4931

y own knowledge are true and that all statement

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may leopardize the validity of the application or any patent issued thereon.

Full Name of Inventor:	Paul A. Boerger	Citizenship:	us
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Paul Q. Bo	erger	3/22/0	0
Inventor's Signature	-0	Date	

DECLARATION AND POWER OF ATTORNEY. ATTORNEY DOCKET NO. 10991888-1 FOR PATENT APPLICATION (continued) Full Name of #2 injurity. Keith Forcest Citizenship:

Residence: 3720 Black Oak Court Loveland CO 80538 Post Office Address Inventor's Signature Date Full Name of # 3 joint inventor: Citizenship: Residence: Citizenship: Citizenship: Residence: Citizenship: Citizenship:
Total Name of # 3 joint inventor: Citizenship: Residence: Post Office Address:
Inventor's Signature Full Name of # 3 joint inventor: Residence: Post Office Address: Inventor's Signature Date Full Name of # 4 joint inventor: Residence: Post Office Address: Inventor's Signature Date Full Name of # 5 joint inventor: Full Name of # 5 joint inventor: Citizenship: Residence: Post Office Address: Inventor's Signature Date Full Name of # 5 joint inventor: Citizenship: Residence: Post Office Address: Inventor's Signature Date
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Full Name of # 5 joint inventor: Residence: Post Office Address: Inventor's Signature Date Full Name of # 6 joint inventor: Citizenship:
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Full Name of # 6 joint inventor: Citizenship:
Full Name of # 6 joint inventor:
Residence:
Post Office Address:
Inventor's Signature Date
Full Name of # 7 joint inventor: Citizenship:
Residence:
Post Office Address:
Inventor's Signature Date
Full Name of # 8 joint inventor: Critizenship:
Full Name of # 8 joint inventor: Citizenship: Residence:
Post Office Address:
Inventor's Signature Date